

## MATERIALS SCIENCE

## Electrically switchable metadevices via graphene

Osman Balci,<sup>1\*</sup> Nurbek Kakenov,<sup>1</sup> Ertugrul Karademir,<sup>2</sup> Sinan Balci,<sup>3</sup> Semih Cakmakyapan,<sup>4</sup> Emre O. Polat,<sup>5</sup> Humeyra Caglayan,<sup>6</sup> Ekmel Özbay,<sup>1,7</sup> Coskun Kocabas<sup>1,\*†</sup>

Metamaterials bring subwavelength resonating structures together to overcome the limitations of conventional materials. The realization of active metadevices has been an outstanding challenge that requires electrically reconfigurable components operating over a broad spectrum with a wide dynamic range. However, the existing capability of metamaterials is not sufficient to realize this goal. By integrating passive metamaterials with active graphene devices, we demonstrate a new class of electrically controlled active metadevices working in microwave frequencies. The fabricated active metadevices enable efficient control of both amplitude (>50 dB) and phase (>90°) of electromagnetic waves. In this hybrid system, graphene operates as a tunable Drude metal that controls the radiation of the passive metamaterials. Furthermore, by integrating individually addressable arrays of metadevices, we demonstrate a new class of spatially varying digital metasurfaces where the local dielectric constant can be reconfigured with applied bias voltages. In addition, we reconfigure resonance frequency of split-ring resonators without changing its amplitude by damping one of the two coupled metasurfaces via graphene. Our approach is general enough to implement various metamaterial systems that could yield new applications ranging from electrically switchable cloaking devices to adaptive camouflage systems.

## INTRODUCTION

Metamaterials have been a powerful tool to control and manipulate electromagnetic waves and their interaction with matter (1–3). The integration of passive metamaterials with a variety of tuning mechanisms has been extensively examined to generate active metadevices that have novel functionalities (4–7). Because of the different tuning mechanisms, these active metadevices can be classified into three general categories, which are circuit-, material-, and physical-based metadevices (8). The circuit-based metadevices use variable capacitors or switches to alter the lumped elements of the equivalent circuit. For instance, the reverse bias voltage applied on a varactor integrated on a split-ring resonator (SRR) changes the effective capacitance of the equivalent circuit (9–12). Material-based metadevices rely on controlling bulk material properties, such as the permittivity, permeability, or conductivity, of the individual unit cell under an external stimulus (7, 13–18). The conductivity of semiconducting material deposited in the split gap can be tuned by illumination and thereby alters the resonance frequency of the metamaterial. Similarly, interconnected metamaterials fabricated on a semiconductor surface have been used to control the depletion area that alters the free-carrier absorption (19, 20). Alternatively, some phase transition materials, such as VO<sub>2</sub>, have been used for altering the resonance behavior of metamaterials (21, 22). By changing the temperature of these materials around the phase transition temperatures, one can control their conductivity and hence the resonance behavior of metamaterials made of or integrated with them. On the other hand, physical metadevices tune their response by changing their shape or

relative position of subcomponents (such as split gap) (23–27). For example, microelectromechanical-based devices can modify the resonance frequency of metadevices in terahertz spectra (25). Although the demonstrated devices provide some degree of tunability, their performances are limited to narrow spectra with a small dynamic range due to the material and fabrication limitations. Therefore, these technologies would greatly benefit from a material that yields large tunability over broad spectra. None of the existing materials provides these challenging requirements. Furthermore, the requirement for electrically controlled tunability places another challenge for practical applications of metadevices.

Two-dimensional (2D) crystals provide new perspectives for reconfigurable smart surfaces that can be used for the realization of electrically tunable metadevices (28–32). The thickness of 2D crystals is much shorter than the effective wavelength; therefore, their electromagnetic response solely originates from the charge carriers. Recent studies have shown that tuning the density of high-mobility free carriers on graphene yields an unprecedented ability to control light-matter interaction over a very broad spectrum ranging from visible to microwave frequencies (33, 34). By engineering the shape or doping level, the plasma frequency of graphene can be tuned between infrared (IR) and terahertz frequencies (30, 35). Notably, the charge density alters the effective dielectric constant of the medium. In another approach, graphene is coated on metamaterials (36, 37) or optical antennas (38, 39) to yield electrically tunable metadevices. However, these devices are not suitable for practical applications due to limited tunability (40). Recently, we discovered a simple device structure consisting of an electrolyte medium sandwiched between two large-area graphene electrodes. This geometry permits an efficient mutual gating between two graphene electrodes that yields charge densities on the order of 10<sup>14</sup> cm<sup>-2</sup> (41). Using this supercapacitor structure, we fabricated various optoelectronic devices, including optical modulators (41, 42), electrochromic devices (43), and switchable radar-absorbing surfaces (44). Here, by using graphene supercapacitors incorporated with metallic SRRs, we demonstrated a new type of electrically tunable metadevices. The fabricated metadevices are based on gate-tunable high-mobility free carriers on graphene, which introduces electrically tunable dissipation in the resonator capacitively coupled to the graphene electrodes.

<sup>1</sup>Department of Physics, Bilkent University, 06800 Ankara, Turkey. <sup>2</sup>School of Physics and Centre for Research on Adaptive Nanostructures and Nanodevices, Trinity College Dublin, College Green, Dublin 2, Ireland. <sup>3</sup>Department of Photonics, Izmir Institute of Technology, 35430 Izmir, Turkey. <sup>4</sup>Electrical Engineering Department, University of California, Los Angeles, Los Angeles, CA 90095, USA. <sup>5</sup>ICFO–Institut de Ciències Fotoniques, The Barcelona Institute of Science and Technology, 08860 Castelldefels, Barcelona, Spain. <sup>6</sup>Laboratory of Photonics, Tampere University of Technology, 33720 Tampere, Finland. <sup>7</sup>Nanotechnology Research Center–NANOTAM, Bilkent University, 06800 Ankara, Turkey.

\*Corresponding author. Email: obalci@fen.bilkent.edu.tr (O.B.); ckocabas@fen.bilkent.edu.tr (C.K.)

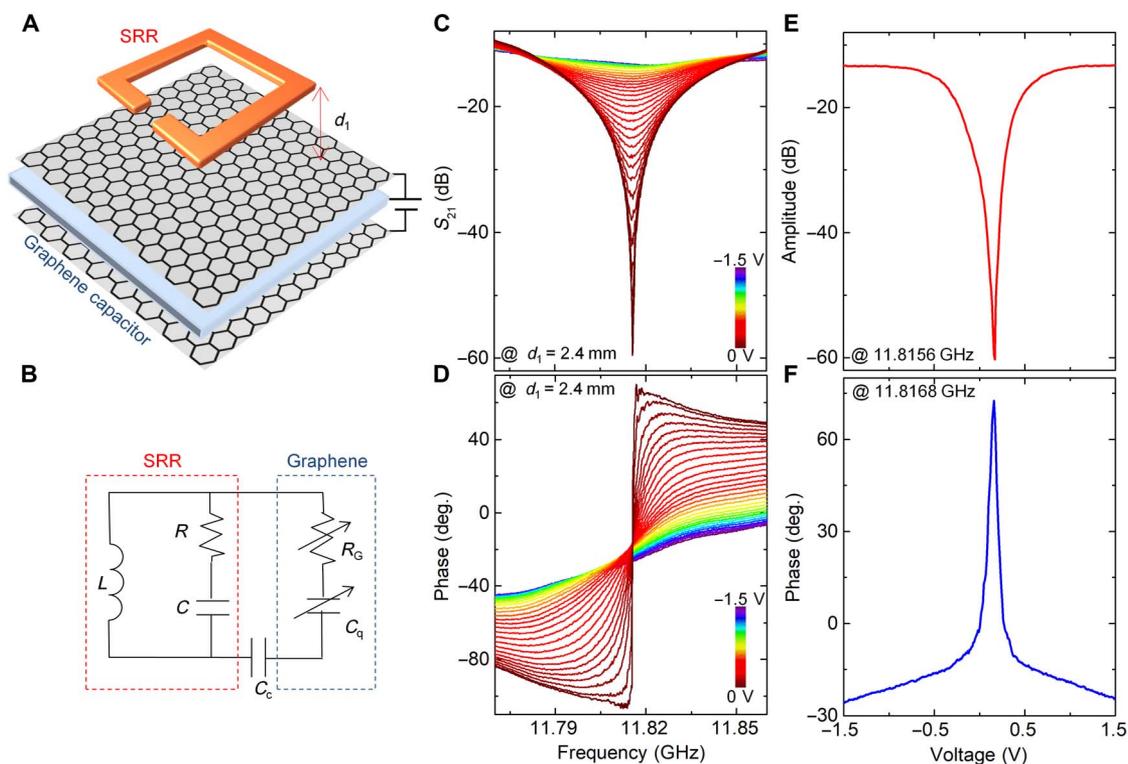
†Present address: School of Materials, University of Manchester, M13 9PL Manchester, UK.

## RESULTS

Integrating SRRs in close proximity to graphene surface yields a new type of hybrid metamaterial whose resonance amplitude can be tuned by various means. Previous attempts to integrate graphene with metamaterials yielded very limited modulation in IR and terahertz frequencies (35, 37). Here, we follow a different approach by using microwave metamaterials capacitively coupled to a large-area graphene that yields substantial tunability. Figure 1A shows a schematic drawing of this hybrid structure. The presence of graphene in close proximity to SRR introduces additional electrical losses due to the sheet resistance of graphene. The equivalent small-signal model of the hybrid structure is shown in Fig. 1B. The ring and split gap provide the inductance,  $L$ , and the capacitance,  $C$ , respectively. The resistor,  $R$ , models the dissipation on the metal due to the electrical and radiation resistance. In our design, the SRR is capacitively coupled to graphene ( $C_c = \frac{\epsilon\epsilon_0}{d}$ , where the coupling capacitance,  $\epsilon$ , is the dielectric constant of the medium and  $\epsilon_0$  is the free-space permittivity). The graphene layer can be modeled by the sheet resistance [ $R_G = \frac{1}{\sigma(n)}$ , where  $\sigma(n)$  is a charge-dependent sheet conductance of graphene], and quantum capacitance of the graphene electrodes ( $C_Q = \frac{2e^2}{h\nu_F} \sqrt{\frac{n}{\pi}}$ , where  $e$  is the elementary charge,  $\nu_F$  is the Fermi velocity, and  $n$  is the charge density). The quantum capacitance of unintentionally doped graphene layer ( $C_Q \sim 0.5 \mu\text{F}/\text{cm}^2$ ) is much larger than the serial coupling capacitance ( $C_c \sim 5 \text{pF}/\text{cm}^2$ ) and therefore, in the small-signal model, we can neglect its contribution (45). Capacitive coupling of a graphene layer to an SRR alters the required total impedance to achieve a resonance in transmitting electromagnetic waves.

Therefore, both the capacitive coupling distance ( $d_1$ ) and the charge density (or bias voltage) on graphene change the resonance condition.

To tune the electrical resonance of metamaterials, we varied the charge density on graphene layer via ionic gating. It should be emphasized here that the technical challenge for graphene-based microwave devices is the requirement of large-area devices owing to the centimeter-scale wavelength (that is,  $\lambda = 3 \text{ cm}$  at 10 GHz). To overcome this challenge, we synthesized large-area graphene by chemical vapor deposition (CVD) on copper foils, which enables us to realize the proposed microwave metadevices (46). Graphene electrodes were synthesized on copper foils using a CVD system, and we subsequently transferred them onto flexible polyvinyl chloride (PVC) substrates by using hot lamination technique. Next, we etched the laminated copper foils in a 5 mM  $\text{FeCl}_3$  aqueous solution. Although CVD synthesis of graphene enables the growth of large-area graphene layers, the quality of graphene may diminish because of the inevitable defects and polymeric residues after the transfer. To fabricate graphene capacitor, we first put a paper tissue with a thickness of  $80 \mu\text{m}$  between two graphene electrodes as a spacer layer, and then we soaked ionic liquid (1-butyl-3-methylimidazolium hexafluorophosphate) into the tissue. The fabricated device structure resembles the supercapacitors formed by single-layer graphene electrodes. The used electrolyte permits mutual electrolyte gating between the graphene electrodes without using any metallic gate electrodes. Under an external bias voltage, the electrolyte is polarized and gates the graphene electrodes. The graphene electrode connected to the negative voltage becomes electron-doped (n-doped), whereas the other one

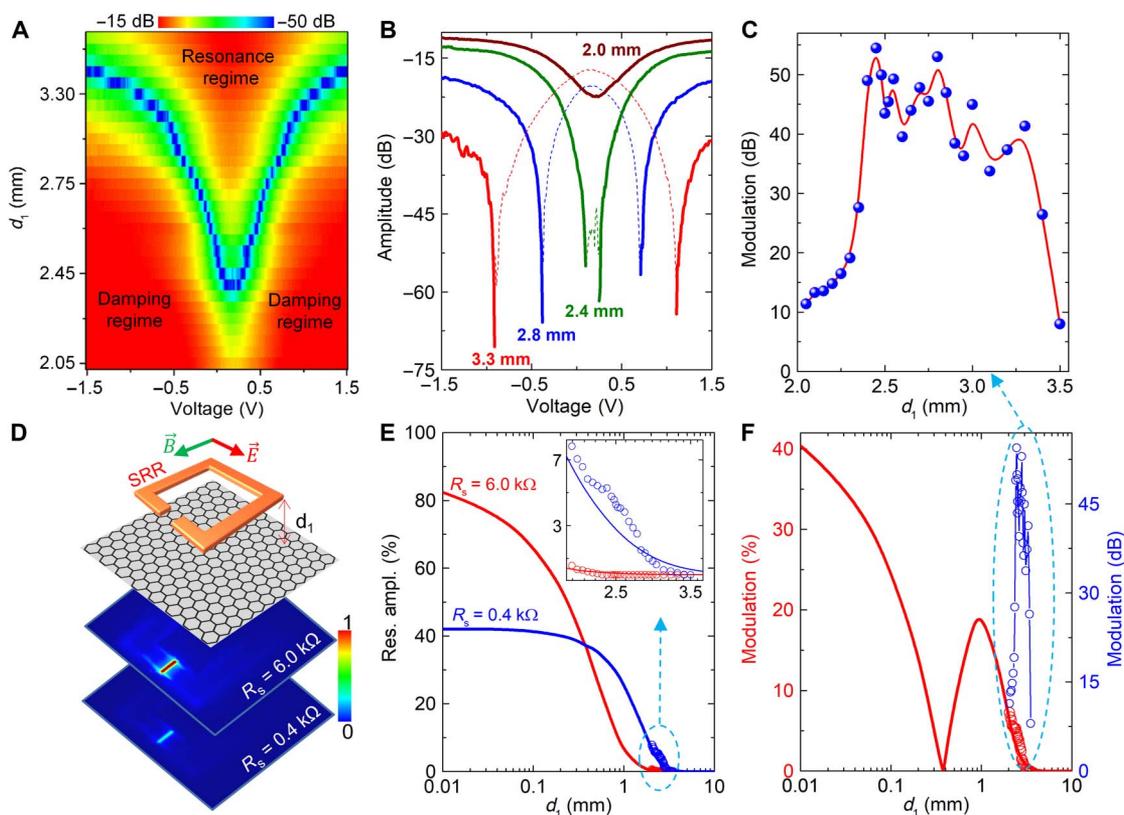


**Fig. 1. Electrically tunable metadevices.** (A) Schematic representation of the hybrid metamaterial system consisting of SRR capacitively coupled to the graphene electrodes. The capacitive coupling is defined by the SRR-graphene separation,  $d_1$ . (B) Small-signal equivalent circuit model of the metadvice. SRR is represented by the  $L$ ,  $R$ , and  $C$  lump circuit elements; the graphene layer is modeled by the variable sheet resistance,  $R_G$ , and quantum capacitance,  $C_Q$ .  $C_c$  models the capacitive coupling. (C and D) Spectra of the magnitude and phase of the transmittance ( $S_{21}$ ) at various bias voltages. The color bar shows the bias voltage. (E and F) The variation of the amplitude and phase of the transmittance with the bias voltage.

becomes hole-doped (p-doped). At 0 V, the sheet resistance of undoped graphene is around 2.5 kilohm and it decreases to 0.7 kilohm at  $\pm 3$  V. The charge density on the graphene electrodes changes between  $3 \times 10^{11}$  to  $0.5 \times 10^{14} \text{ cm}^{-2}$ . The metallic SRRs were fabricated on another PVC film by printing the SRR shapes on previously laminated 10- $\mu\text{m}$ -thick copper foil followed by the chemical etching of copper. Detailed explanation of device fabrication and characterization procedures are all presented in section S1. After assembling the device, we measured the scattering parameters using a broadband horn antenna as a source and a monopole antenna as a receiver connected to a two-port network analyzer. To excite the electrical resonance, we polarized the electric field along the split gap of SRR. The active device yields an unprecedented ability to control the intensity and phase of the transmitted electromagnetic waves. In actuality, Fig. 1 (C and D) shows the amplitude and phase of the transmittance ( $S_{21}$ ) measured through the fabricated device at various bias voltages at  $d_1 = 2.4$  mm, respectively. Here,  $d_1 = 2.4$  mm is the critical capacitive coupling distance ( $d_c$ ) between the SRR arrays and graphene capacitor, resulting in a maximum modulation of resonance amplitude in decibel scale with bias voltage. At 0 V, the device yields a resonance at 11.8156 GHz with a resonance transmittance of  $-60$  dB. When we applied a bias voltage, electrons and holes accumulate on the graphene electrodes and yield significant

damping that diminishes the resonant behavior. For example, at 1.5 V, the resonance transmittance is  $-12$  dB. Figure 1 (E and F) shows the voltage dependence of the amplitude of transmittance at resonance (11.8156 GHz) and the phase (at 11.8168 GHz). The phase of the transmitted signal varies from  $-30^\circ$  to  $70^\circ$ . We observed a symmetric behavior when we changed the polarity of the bias voltage owing to the ambipolar behavior of the graphene electrodes. Notably, the charge neutrality point is slightly shifted to positive voltages due to the slight chemical doping of graphene by polarized ionic liquid. The shift can be minimized by waiting longer during the voltage scan. More details about the microwave performance of our metadvice are explained in section S2.

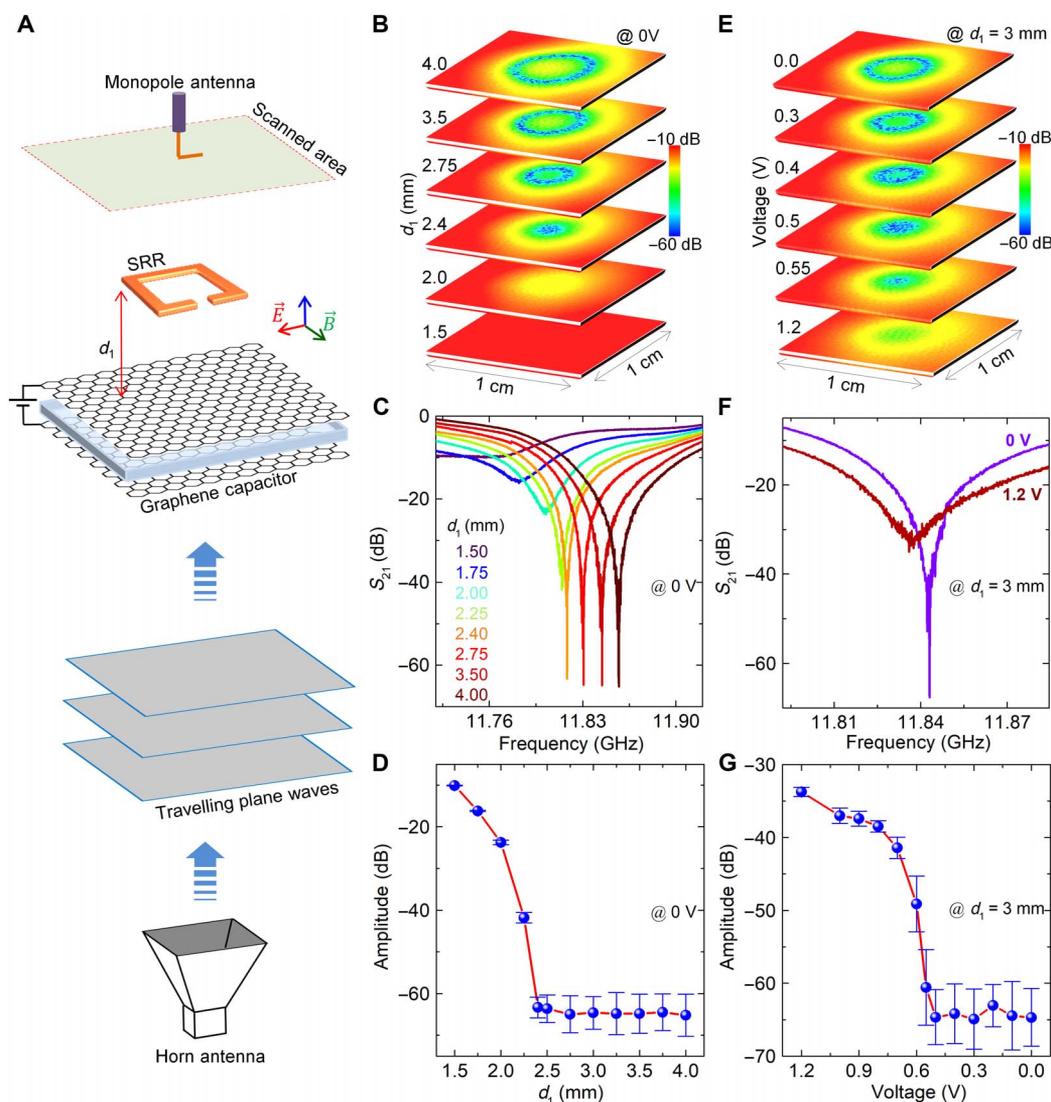
To understand the effect of the separation ( $d_1$ ) between graphene capacitor and metamaterial arrays on the performance of our metadvice, we measured near-field transmission spectrum in the forward direction at various  $d_1$  values while sweeping the bias voltage between  $\pm 1.5$  V. Figure 2A shows the resonance amplitude as a function of  $d_1$  and applied bias voltage. We separate the color plot in two regimes: resonance and damping regimes. In resonance regime (above the blue regions), the SRR is not resonating in the forward direction; therefore, the amplitude increases as  $d_1$  goes above  $d_c = 2.4$  mm. The SRR is resonating in the resonance regime, but the extinction pattern is not at the



**Fig. 2. Investigating coupling distance dependence ( $d_1$ ) of the metadvice performance.** (A) Variation of the resonance amplitude (Res. ampl.) with  $d_1$  and bias voltage in the forward direction. Although the bias voltage damps the resonance at the damping regimes, it changes the radiation pattern of SRRs without changing its amplitude in the resonance regimes. (B) Resonance amplitude as a function of bias voltage at various  $d_1$ , extracted from (A). The solid lines represent damping and dash lines represent resonance regimes. (C) Modulation of transmission amplitude at resonance with bias voltage as a function of  $d_1$ . Modulation is maximum at  $d_c = 2.4$  mm. (D) Schematic drawing for the metadvice structure used in finite element simulation together with simulated electric field distribution on SRR at 6- and 0.4-kilohm sheet resistance ( $R_s$ ) of single-layer graphene at  $d_1 = 2$  mm. (E) Simulated variation of resonance amplitude of SRR arrays with  $d_1$  for  $R_s = 6$  and 0.4 kilohm. The inset shows calculated resonance amplitude variation with experimentally measured ones. (F) Simulated and measured resonance amplitude modulation as a function of  $d_1$ . The blue scattered circles are experimentally measured amplitude modulation in decibel scale.

position of the monopole antenna. It should be emphasized here that the variation in the near-field extinction pattern of SRRs is presented in more detail in Fig. 3. First, the extinction pattern of the SRR is collected toward the antenna position at a critical bias voltage ( $V_c$ ), and subsequently, the damping starts beyond that voltage in the damping regimes. The blue regions in Fig. 2A show that  $d_1$  and  $V_c$  condition together to achieve a resonance having an amplitude below  $-50$  dB in the forward direction at the position of the monopole antenna. In the damping regimes (below the blue region in Fig. 2A), the SRR is always resonating in the forward direction; hence, applied bias voltage damps its resonance. Figure 2B shows line plots of the variation in the resonance amplitude with the applied bias voltage for some  $d_1$  values, extracted from Fig. 2A. Here, the straight lines represent the damping regime, and the dash lines represent the resonance regime. Resonance amplitude below  $-50$  dB can be achieved for  $d_1 \geq d_c$ , and the resonance can be damped with the bias voltages above  $V_c$  (varies for each  $d_1 \geq d_c$ ).

To find the modulation of the resonance amplitude with the bias voltage, we compare the resonance amplitude at  $\pm 1.5$  V and  $V_c$  for each  $d_1$  values. We have achieved the maximum modulation of 55 dB at  $d_c = 2.4$  mm (Fig. 2C). The modulation increases very fast for  $d_1 < d_c$  and decreases slowly for  $d_1 > d_c$ . More detailed measurements and analysis for the experimental characterization of the coupling distance ( $d_1$ ) are presented in section S2. To further investigate the effect of  $d_1$  on the performance of our metadvice, we simulate our device in a finite element simulation platform (COMSOL) using the device structure shown in Fig. 2D. We used a single-layer graphene and an SRR coupled to that graphene at  $d_1$  in the unit cell. The color plots in Fig. 2D show the normalized electric field intensities on the SRR for 6.0 and 0.4 kilohm sheet resistances ( $R_s$ ) of the single-layer graphene. The field is confined in the split gap, and doping the single-layer graphene decreases the intensity of the electric field. Then, we calculate the resonance amplitude of the SRR as a function of  $d_1$  for 6.0 and 0.4 kilohm  $R_s$  values



**Fig. 3. Near-field characterization of the active metadvice.** (A) Near-field scanning technique to map the local scattering parameter ( $S_{21}$ ) of the device. Scattering parameter provides the magnitude of the local electric field along the direction of the antenna. (B to D) Spatial map, spectrum, and average resonance amplitude of the local scattering parameter of the metadvice probed by a monopole antenna at different graphene-SRR distances at 0 V. (E to G) Voltage dependence of the spatial map, spectrum, and resonance amplitude of the local scattering parameters of device at  $d_1 = 3$  mm.

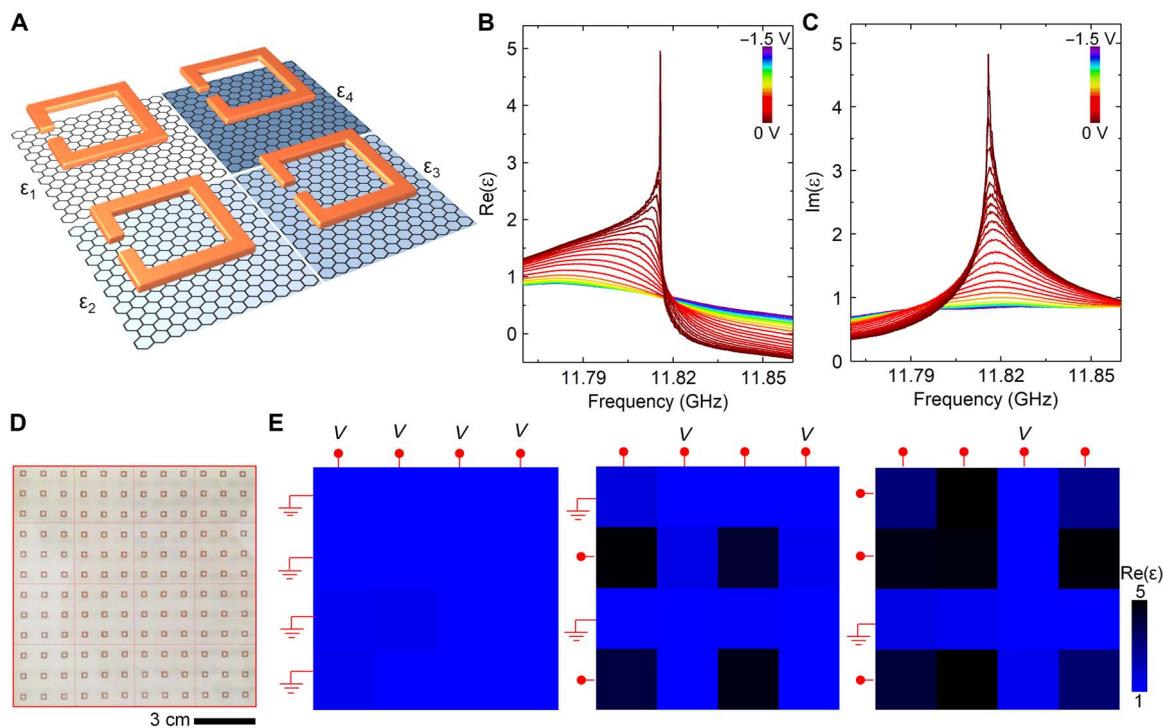
(Fig. 2E). The amplitudes for both  $R_s$  values are decreasing with  $d_1$  due to the variation in the coupling capacitance. The scattered circles in Fig. 2E and the inset show the measured resonance amplitudes of our metadvice for doped and undoped cases. As a result, there is good agreement between the simulation and the experimental data. Using the calculated resonance amplitudes, we calculate the modulation of the amplitude in percentage (%) scale as a function of  $d_1$  (Fig. 3F). The global maximum is achieved at very short  $d_1$  values (at 0 mm) and the local maximum is at  $d_1 = 1$  mm. Our measured modulation in percent scale follows the calculated one very well for  $d_1$  values used in the experiments. Using the same strategy used for simulation of the metadvice working in the microwave frequencies, we simulated the performance of graphene to control the resonance amplitude of SRRs from terahertz to visible frequencies. We have found the critical coupling distances to achieve maximum modulation in their amplitude both in decibel and percent scales. Detailed results of the simulations performed from microwave to visible frequencies are presented in section S3. As a result of the simulations performed, we conclude that our approach is valid from microwave to visible frequencies in the electromagnetic spectrum.

To explore the tunability of electric field distribution of active metadvice, we used a near-field scanning technique to map the local electric field distributions (47). We placed the device on a computer-controlled motorized stage and recorded the spectrum of local scattering parameter by using a monopole antenna connected to a network analyzer (Fig. 3A). First, we examined the critical coupling condition between the graphene electrode and SRR at zero bias voltage. Figure 3B shows the measured local transmission ( $S_{21}$ ) intensity distribution of metadvice at different graphene-SRR separation. In the near-field of the metadvice, the complete extinction of the microwave signal (that

is, resonance) occurs on a ring-shape region whose radius depends on the graphene-SRR separation. When graphene is very close ( $<2$  mm) to the SRR, the resonance diminishes because of the large dissipation on graphene. Figure 3C shows the transmittance spectrum, and Fig. 3D shows the average resonance amplitude at different  $d_1$  values at 0 V. The resonance depth decreases with an increase in  $d_1$  and stays nearly constant for  $d_1$  values larger than the critical coupling distance ( $d_c$ ) of 2.4 mm. We are limited with the noise level of our measurement system. Then, we measured the variation of the near-field distribution as a function of bias voltage at  $d_1 = 3$  mm (Fig. 3E). Upon increasing the charge density on graphene electrodes, the extinction ring shrinks further and diminishes at large voltages. The transmission spectra at 0 and 1.2 V are demonstrated in Fig. 3F. Although the size of the extinction pattern becomes smaller until a critical bias voltage ( $V_c$ ) of 0.55 V, the resonance amplitude does not change and it is damped beyond that voltage. The critical bias voltage to start damping increases with the separation distance for  $d_1 \geq d_c$ . More details about the imaging near-field extinction pattern of SRRs are presented in section S4.

## DISCUSSION

To show the promise of the approach, now we would like to demonstrate the spatial tuning of metamaterials that could open new applications in transformation optics (48). Transformation optics is an emerging field of research aiming to conceal an object by bending or distorting electromagnetic waves using spatially varying metamaterials (49, 50). The ability to control the spatial variation of permittivity and permeability by electrical means would yield new perspectives on adaptive electromagnetic cloaking and camouflage. By integrating arrays of individually

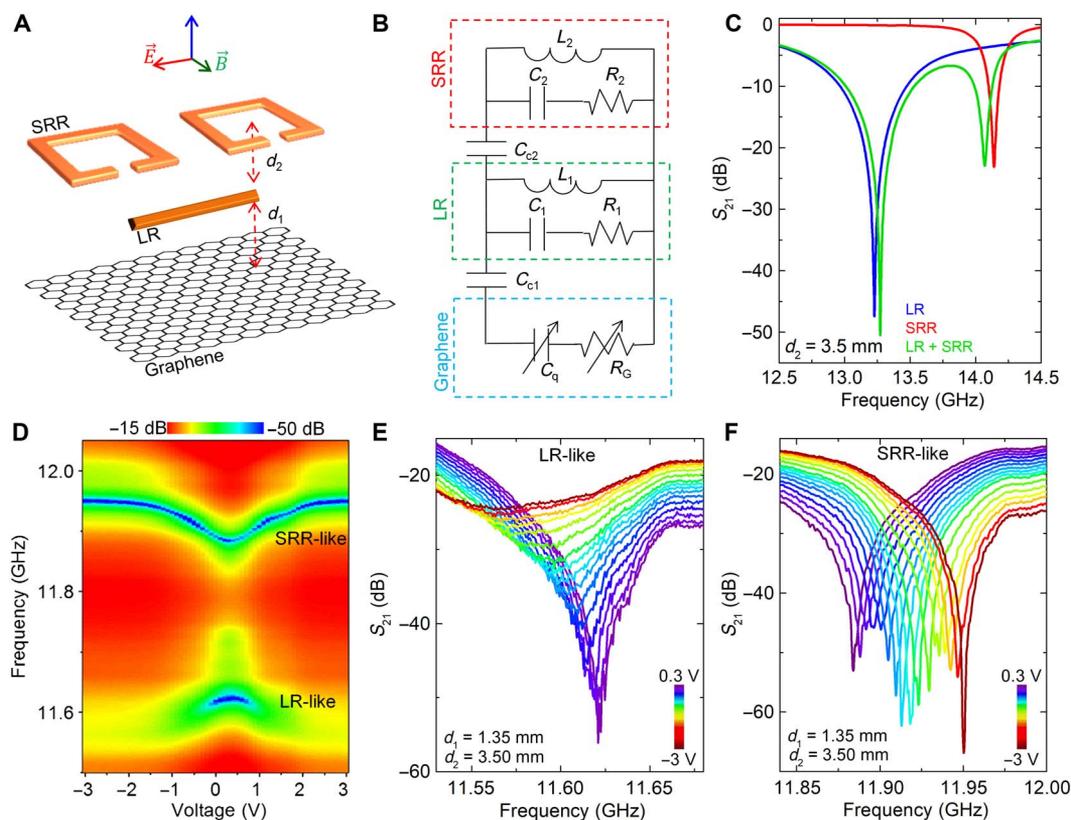


**Fig. 4. Electrically reconfigurable, spatially varying digital metamaterials.** (A) Schematic drawing of a digital metamaterial with individually addressable pixels. Controlling the charge density on individual pixels allows us to reconfigure the local dielectric constant. (B and C) The spectra of the calculated real and imaginary part of the effective dielectric constant of a single pixel under different bias voltages. (D and E) The spatial map of the real part of the effective dielectric constant of the device at the resonance condition for different voltage configurations. The effective dielectric constant of the pixels is controlled by passive matrix addressing.

addressable metadevices, our approach can be used for voltage-controlled adaptive transformation optics. Figure 4 shows the schematic of the multipixel device. By controlling the local charge density on a pixelated surface by passive matrix addressing, we demonstrate an electrically reconfigurable, spatially varying metadevices. We fabricated a large-area metadevice with  $4 \times 4$  arrays of active pixels. Each pixel contains nine SRRs ( $3 \times 3$ ). We measured the scattering parameter at the center of the pixels and then calculated the local dielectric function. To calculate the dielectric function, we first write the  $S$  parameters in terms of impedance and refractive index of the metasurface and calculated their roots in terms of  $S$  parameters, as given by Chen *et al.* (51). To overcome the branching problem for the real part of the refractive index, we used Kramers-Kronig relations, as developed by Szabo *et al.* (52). We used our unit cell size of 11 mm for the effective thickness of our metamaterial structure. Figure 4 (B and C) shows the calculated real and imaginary part of the effective dielectric constant. By accumulating charges on a pixel, the local dielectric constant varies from 5 down to 0.8. Figure 4 (D and E) shows spatial maps of the real part of the dielectric constant of the pixelated device at different voltage configurations. Details for the spatially varying metadevices are explained in section S5. We were able to reconfigure the spatial variation of the dielectric constant over the device by precisely varying the voltage applied to the rows and columns. It is necessary to point out here that the cross-coupling between the pixels is due to the passive matrix addressing. The fabricated devices are on thin flexible sub-

strates, and therefore, they can be wrapped around nonplanar objects for cloaking applications.

Tuning resonance frequency of a metasurface without modifying its amplitude is one of the challenges for active metadevices. To overcome this challenge, we have implemented a unique metadevice concept to actively control the resonance frequency of the device by electrical means. The metadevice consists of three coupled layers: the first is SRR, second is line resonator (LR) arrays, and third is the graphene capacitor. We used large-area graphene capacitor as an electrically tunable active component of the metadevice. The unit cell of the metadevice is schematically illustrated in Fig. 5A, where two SRRs are coupled to a single LR at  $d_2$  and both of them are coupled to a graphene capacitor at  $d_1$  below the LR. Note that each layer is coupled capacitively to each other, and the coupling capacitance is proportional to the distance between them. Small-signal circuit model of the entire metadevice with electrostatic-coupling capacitances are shown in Fig. 5B. Graphene is represented with a tunable quantum capacitance ( $C_q$ ) and sheet resistance ( $R_s$ ). Uncoupled single layer of SRR and LR surfaces have their own resonance dips in transmission spectrum; simulated results are shown in Fig. 5C. Coupling these layers at  $d_2 = 3.5$  mm results in two resonance dips, where one resonance is SRR-like and the other resonance is LR-like. LR-like resonance is at higher frequencies, and SRR-like resonance is at lower frequencies than the uncoupled states. Our aim here is to actively tune the SRR-like resonance frequency, without changing its amplitude, by selectively damping the LR-like resonance. Therefore, we placed the



**Fig. 5. Frequency-tunable active metadevices.** (A) Schematic drawing of the designed three-layer frequency-tunable metadevice structure. In a unit cell, two SRRs are coupled to a LR at  $d_2$ , and a graphene capacitor is coupled to both of them at  $d_1$  below the LR layer. (B) Small-signal circuit model to represent the three-layer metadevice. (C) Transmission spectrum showing the resonances of coupled ( $d_2 = 3.5$  mm) and uncoupled SRR and LR metasurfaces. (D) Experimentally measured variation in the transmission spectrum of the three-layer metadevice by means of bias voltages applied to graphene capacitor at  $d_1 = 1.35$  mm and  $d_2 = 3.50$  mm. (E) Transmission spectrum showing the resonance damping of LR-like resonance with bias voltage. (F) Transmission spectrum showing the shift in the frequency of the SRR-like resonance with bias voltages without varying its amplitude.

graphene capacitor closer to the LR layer than the SRR layer. Transmission spectra measured from the three-layer metadvice as a function of bias voltages are shown in Fig. 5D for  $d_1 = 1.35$  mm and  $d_2 = 3.50$  mm. The regions with blue color show the resonance amplitude below  $-50$  dB. Charging graphene capacitor with bias voltages damps the resonance amplitude of the LR-like resonance (Fig. 5E) while shifting the resonance frequency of the SRR-like resonance (Fig. 5F). The amplitude of the SRR-like resonance fluctuates with applied bias voltages, but its overall amplitude stays below  $-50$  dB level. We have obtained a similar active frequency-tunable metadvice by coupling two uniform SRR layers (see section S6).

## CONCLUSION

The results presented here confirm a promising approach for electrically controlled active metadivices. The core idea of the approach is based on the electrical tuning of effective strength of a resonator placed close to a tunable Drude metal. Electrostatic tuning of the charge density on graphene yields broadband controllability on the response of various types of metamaterials both in near- and far-field (sections S7 and S8). These active metadivices enable efficient control of both amplitude ( $>50$  dB) and phase ( $>90^\circ$ ) of electromagnetic waves. To show the promising uses of the approach, we demonstrated electrically reconfigurable spatially varying metamaterials and frequency-tunable active metadivices. The operation frequency of these metadivices can be easily scaled up to the terahertz and higher frequencies. Large modulation depth, simple device architecture, and mechanical flexibility are the key attributes of the graphene-enabled active metadivices. We anticipate that the presented approach could lead to new applications ranging from electrically switchable cloaking devices to adaptive camouflage systems in microwave and terahertz frequencies.

## MATERIALS AND METHODS

### Fabrication of graphene capacitors

We synthesized large-area ( $7 \times 14$  cm<sup>2</sup>) graphene using a CVD system on ultrasmooth copper foils (Mitsui Mining and Smelting Company, Ltd, B1-SBS) under 100 sccm H<sub>2</sub> and 10 sccm CH<sub>4</sub> flow for 1 min at 1035°C. After the growth, we transferred the graphene on a flexible 75- $\mu$ m-thick PVC substrate using hot lamination technique. After etching the Cu in 5 mM aqueous solution of FeCl<sub>3</sub>, we used two layers of graphene on PVC to fabricate a large-area graphene supercapacitor. A paper tissue with a thickness of 100  $\mu$ m was used as a spacer between two graphene electrodes. We first put the tissue on top of one graphene electrode and then ionic liquid (1-butyl-3-methylimidazolium hexafluorophosphate). We placed the top graphene electrode and let the ionic liquid disperse between the two graphene electrodes.

### Fabrication of metamaterials

To fabricate metamaterial structures, we laminated a 75- $\mu$ m-thick PVC laminating film on 10- $\mu$ m-thick copper foils. We printed the metamaterial structure on the copper foils using Hewlett-Packard Color LaserJet printer (CP2020). We etched the copper in a nitric acid solution. The printed toner functions as an etch mask on copper. With this technique, we can define metadivices having a feature size as small as 80  $\mu$ m.

### Microwave measurements

We used a Keysight E5063A network analyzer for the microwave characterization of our device. For near-field measurements, we connected a horn antenna to one channel and a 1.5-cm-long monopole antenna to

the other channel of the network analyzer to measure the  $S$  parameters ranging from 7 to 15 GHz. The active metadvice was placed at a specific distance above the monopole antenna, and the horn antenna was used to propagate microwaves in free space. The device is placed on a computer-controlled motorized stage with 1- $\mu$ m spatial resolution. Both the amplitudes and phases of the received signals were recorded for each location. The monopole antenna was aligned along the electric field of the horn antenna. We connected the Keithley 2400 source measure unit to apply voltage bias. We tuned the voltage manually and recorded the scattering parameters. For far-field measurements, we used a horn antenna instead of a monopole antenna and placed our devices between two horn antennas to measure far-field  $S$  parameters.

## SUPPLEMENTARY MATERIALS

Supplementary material for this article is available at <http://advances.sciencemag.org/cgi/content/full/4/1/eaao1749/DC1>

- section S1. Fabrication and characterization of graphene supercapacitors
- section S2. Microwave performance of active metadivices in near-field
- section S3. Electromagnetic modeling and simulation of active metadivices
- section S4. Imaging near-field extinction pattern of a square SRR
- section S5. Electrically reconfigurable, spatially varying digital metamaterials
- section S6. Frequency-tunable active metadivices
- section S7. Performance of active metadivices in far field
- section S8. Microwave performance of various metadivices in near-field
- fig. S1. Image of growth, transfer, and etching processes.
- fig. S2. Characterization of single-layer graphene.
- fig. S3. Large-area graphene supercapacitor and its characterization.
- fig. S4. Fabrication of large-area SRR structures.
- fig. S5. Near-field microwave measurement setup.
- fig. S6. Modulation of resonance amplitude in percent scale.
- fig. S7. Modulation of resonance amplitude in decibel scale.
- fig. S8. Detailed analysis for electrical switching of square SRRs.
- fig. S9. Time response of the metadivices.
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## Electrically switchable metadevices via graphene

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